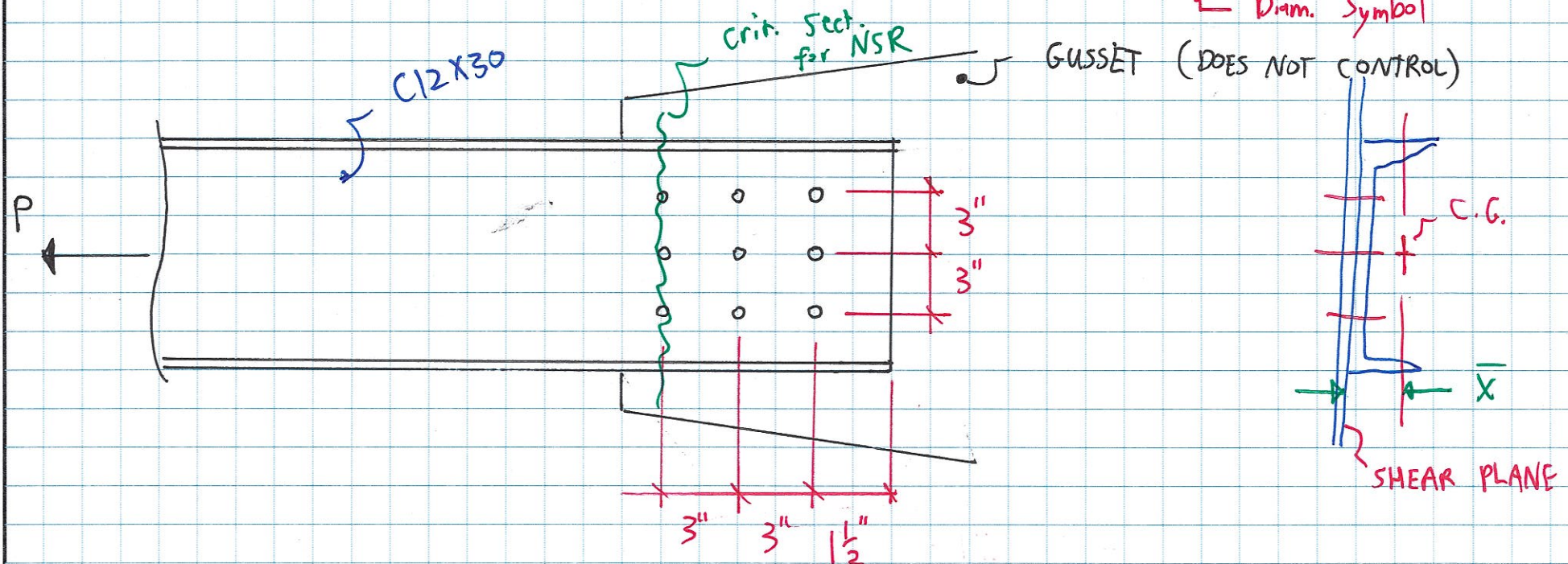


EXAMPLE

GIVEN: A SINGLE C12X30, A36 STEEL, CONNECTED TO A PLATE W/ $\frac{3}{4}$ " ϕ BOLTS



REQ'D: COMPUTE THE DESIGN TENSILE STRENGTH OF THE CHANNEL

SOLN: C12X30: $A_g = 8.81 \text{ in}^2$
 $t_w = 0.51 \text{ in}$
 $\bar{x} = 0.674 \text{ in}$

A36: $f_y = 36 \text{ ksi}$
 $f_u = 58 \text{ ksi}$

GSY: $\phi P_n = \phi f_y A_g = 0.9 (36 \text{ ksi}) (8.81 \text{ in}^2) = \underline{\underline{285.4 \text{ k}}}$

NSR: $\phi P_n = \phi F_u A_e$

$$A_n = A_g - \sum A_{\text{holes}} = 8.81 \text{ in}^2 - (3 \text{ holes}) (0.51") \left(\overset{\substack{\text{tw} \\ \downarrow}}{\frac{3}{4}"} + \overset{\substack{\text{damage} \\ \downarrow}}{\frac{1}{16}"} + \overset{\substack{\text{tolerance} \\ \downarrow}}{\frac{1}{16}"} \right)$$

$$= 7.471 \text{ in}^2$$

$$A_e = U A_n = 0.887 (7.471 \text{ in}^2) = 6.632 \text{ in}^2$$

CASE 2
"General Case"

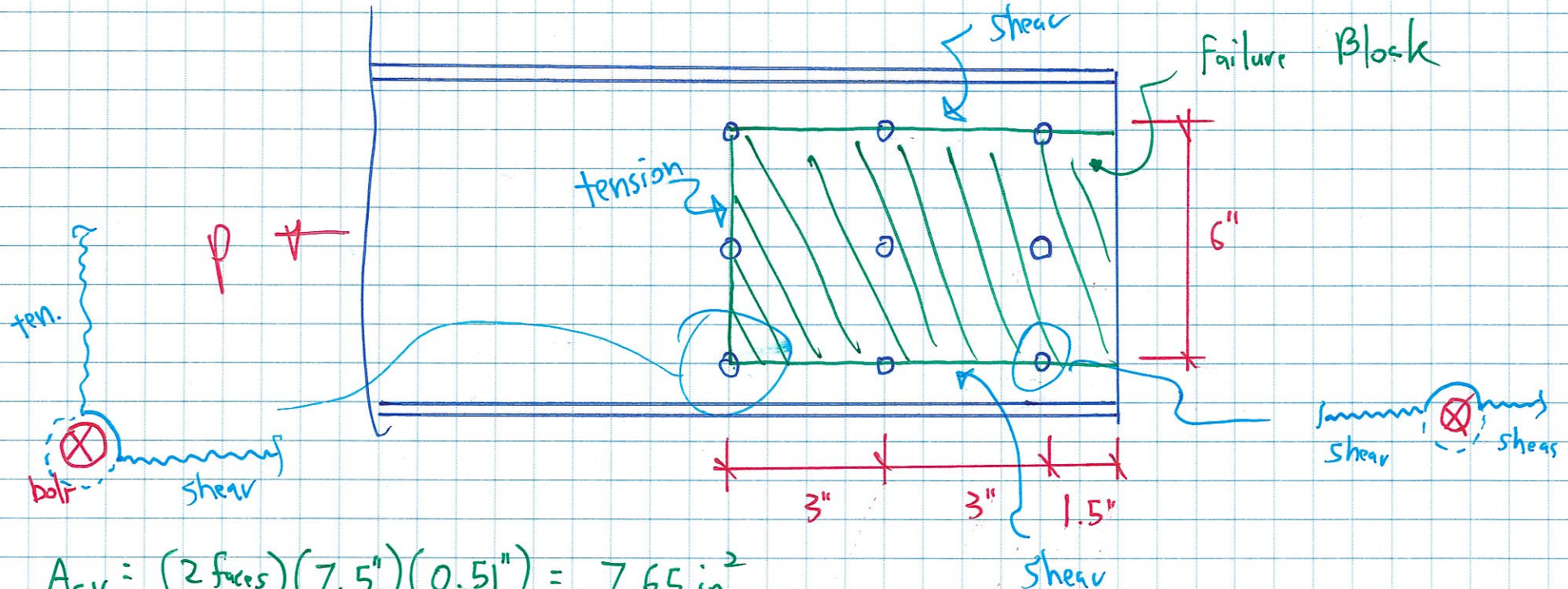
$$U = 1 - \frac{\bar{x}}{l} = 1 - \frac{0.674"}{6"} = 0.887$$

$$\phi_t P_n = 0.75 (58 \text{ ksi}) (6.632 \text{ in}^2) = \underline{\underline{288.5 \text{ k}}}$$

BSR

$$\phi R_n = \phi [0.6F_u A_{nv} + U_{bs} F_u A_{nt}] \leq \phi [0.6F_y A_{gv} + U_{bs} F_u A_{nt}]$$

minimum of the two eqns.



$$A_{gv} = (2 \text{ faces})(7.5'')(0.51'') = 7.65 \text{ in}^2$$

$$A_{nv} = A_{gv} - \sum A_{\text{holes}} = 7.65 \text{ in}^2 - (2 \text{ faces})(2.5 \text{ holes})\left(\frac{3}{4}'' + \frac{1}{8}''\right)(0.51'') = 5.42 \text{ in}^2$$

$$A_{nt} = (6'')(0.51'') - (2 \text{ holes})\left(\frac{3}{4}'' + \frac{1}{8}''\right)(0.51'') = 2.1675 \text{ in}^2$$

$$\phi R_n = 0.75 \left[0.6(58)(5.42 \text{ in}^2) + 1.0(58)(2.168 \text{ in}^2) \right]$$

$$\leq 0.75 \left[0.6(36 \text{ ksi})(7.65 \text{ in}^2) + 1.0(58 \text{ ksi})(2.168 \text{ in}^2) \right]$$

$$\phi R_n = 236^k \leq 218^k$$

↖ Controls

LIMIT STATES

GSY ϕ

$$\phi_t P_n = 285^k$$

NSR

$$\phi_t P_n = 288^k$$

BSR

$$\phi R_n = 218^k \leftarrow \text{CONTROLS}$$

$$\phi P_n = 218^k$$

DESIGN OF TENSION MEMBERSAPP. LIMIT STATES

- 1) GSY
- 2) NSR
- 3) BSR

SERVICEABILITY CHECK: $\left(\frac{L}{r_{\min}} \leq 300 \right)$ { PREVENT EXCESSIVE DEFORMATIONS,
VIBRATIONS, DAMAGE IN TRANSPORT,
CONSTRUCTION

where L is the overall length (in.)

$r_{\min}$ is the minimum radius of gyration

$$\sqrt{I/A}$$

DESIGN PROCESS (Recommendation)

1) Determine $(A_g)_{req'd}$ based on GSY

$$(A_g)_{req'd} \geq \frac{P_u}{0.9 f_y} \quad \leftarrow \text{factored controlling LC}$$

2) Select a member w/ $A_g \geq (A_g)_{req'd}$ from Sect. Properties

3) Compute A_n , U , A_e , & check NSR

4) Check BSR, compute, A_{nt} , A_{gv} , A_{nc}

5) Check $\frac{L}{r_{min}} < 300$

6) Revise member size as necessary by controlling Limit State

* CVEN 446 $\rightarrow$ Select the lightest section:

Assume lightest is cheapest

EXAMPLEGIVEN: A 20-ft Long W-Section, A992 Steel

$$P_L = 20^k$$

$$L_L = 75^k$$

$$P_u = 1.2 \left(\cancel{20^k} \right) + 1.6 (75^k) = 144^k$$

REQ'D: Select the lightest W8X _____ to carry the load, assume BSR & NSRSOLN: A992: $\left. \begin{array}{l} f_y = 50 \text{ ksi} \\ f_u = 65 \text{ ksi} \end{array} \right\}$ Table 2-4, p2-48 AISC do not control.

$$(A_g)_{\text{req'd}} = \frac{P_u}{0.9 f_y} = \frac{144^k}{0.9 (50 \text{ ksi})} = 3.2 \text{ in}^2$$

$$\text{try W8X13: } A_g = 3.84 \text{ in}^2 \approx (A_g)_{\text{req'd}} = 3.2 \text{ in}^2 \therefore \text{GSY OK}$$

$$r_y = r_{\min} = 0.843''$$

$$\frac{L}{r_{\min}} = \frac{(20')(12)}{0.843''} = 284.7 < 300 \quad \checkmark$$

"SERVICEABLE
CHECK"