

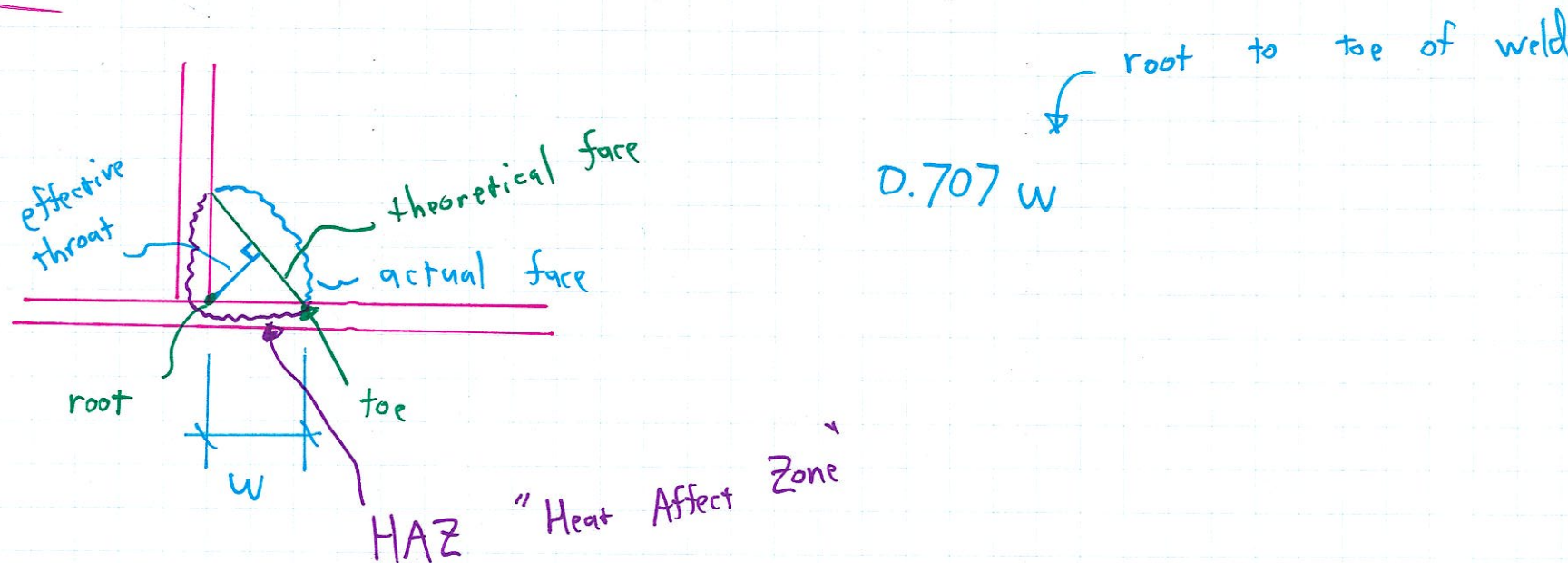
## WELDED CONNECTIONS

\* KEATING MODULE FOR MORE DETAILS

AISC CHAP 5, pg 16.1 - 116

AWS (American Weld Society) D1.1 "Structural Welding Code" governs except as noted in J2

## FILLETS



STRENGTH OF WELD IS DEPENDENT ON

$$1) \text{ BASE MATERIAL} \quad \phi F_{bm} A_{bm} \quad (J2-5)^2$$

$$2) \text{ WELD} \quad \phi F_w A_w \quad (J2-3)$$

FILLET WELD STRENGTH

$$\text{WELD SHEAR STRENGTH: } \phi r_n = 0.75 \left( \underbrace{0.707 w}_{A_w} \times \underbrace{0.6 F_{exx}}_{F_w} \right) \quad (\text{per inch of weld})$$

$$\text{BASE METAL STRENGTH: } \phi r_n = \min \left[ 1.0 (0.6 f_y t) ; 0.75 (0.6 f_u t) \right]$$

\* Smallest controls

where:  $w$  = weld size

$F_{exx}$  = electrode strength

CVEN 446  $\rightarrow F_{exx} = 70 \text{ ksi}$

$F_y, F_u$  = base metal properties

$t$  = thickness of base metal



AISC ALLOWS THE LARGER OF

(i)  $R_n = R_{wl} + R_{wt}$

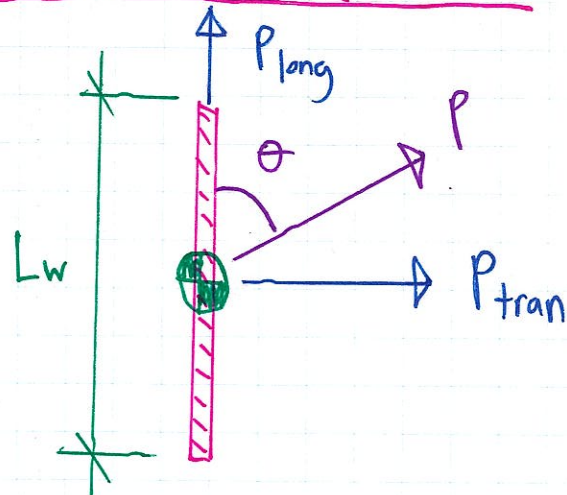
(ii)  $R_n = 0.85 R_{wl} + 1.5 R_{wt}$

\* use largest

$R_{wl} = \text{nom. strength of long. weld}$   
 $= 0.6 F_{exx} (0.707 w) (L_{ew})$  "kip"

$R_{wt} = \text{nom. strength of tran. weld}$   
 $= 0.6 F_{exx} (0.707 w) (L_{tw})$  "kip"

FILLET WELDS @ ANGLES



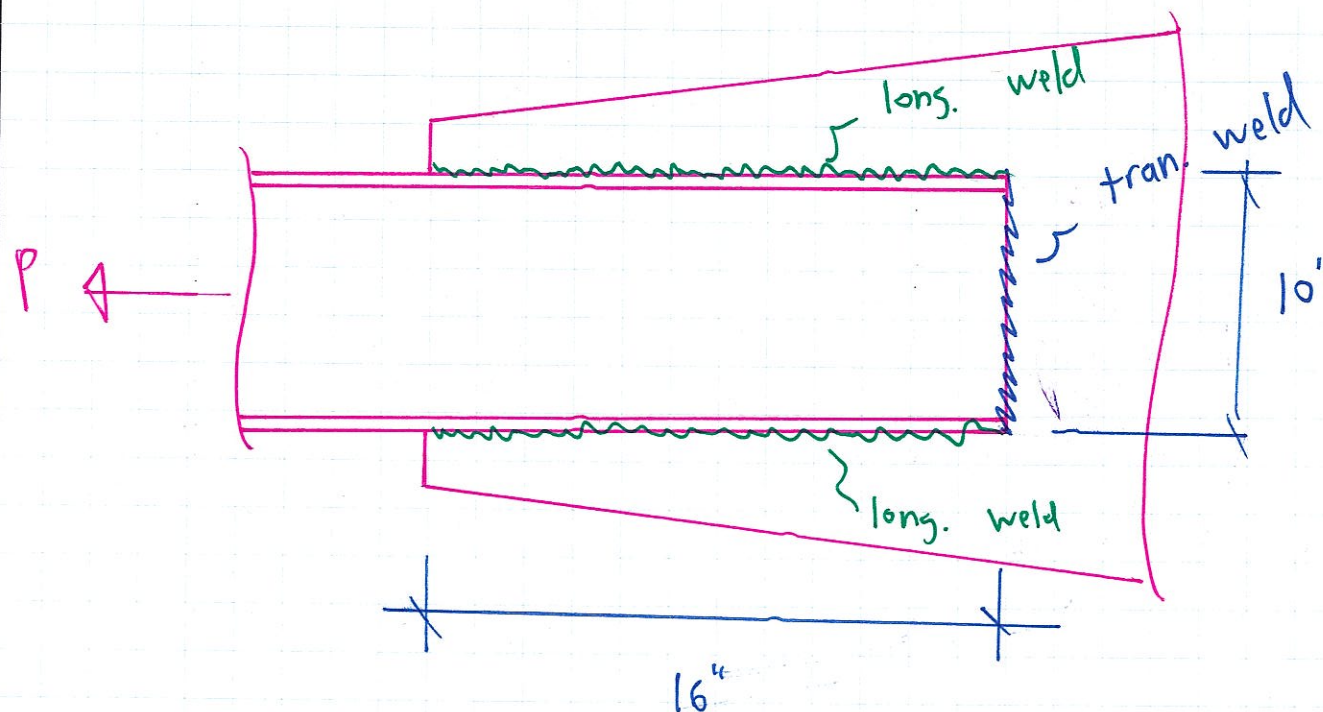
$$F_{nw} = 0.6 F_{exx} (1.0 + 0.5 \sin^{1.5} \theta)$$

$$\phi r_n = 0.75 F_{nw} A_w$$

$0.707 w$

EXAMPLE

GIVEN: A MC10X22, A992 Steel, Member welded to  $\frac{3}{8}$ " gusset, A36 steel, with  $\frac{3}{16}$ " fillet weld, E70 electrodes.

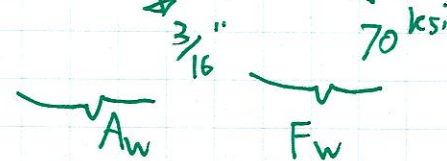


REQD: Determine the connection capacity, not considering member strength

SOLN:



WELD:  $\phi r_n = 0.75 (0.707 w) (0.6 F_{exx}) = 4.176 \text{ k/in}$  "weld shear strength"



BASE METAL:  $\phi r_n = \min [1.0 (0.6 f_y t); 0.75 (0.6 f_u t)]$   
 $= \min [1.0 (0.6) (36 \text{ ksi}) (\frac{3}{8} \text{ in}); 0.75 (0.6) (58 \text{ ksi}) (\frac{3}{8} \text{ in})]$   
 $= 8.1 \text{ k/in}$

smaller controls  $\Rightarrow \phi r_n = 4.176 \text{ k/in}$  since weld strength controls 2 cases

(i)  $\phi R_n = \phi R_{wx} + \phi R_{wt} = 4.176 \text{ k/in} [2 \text{ welds } (16 \text{ in}) + 10 \text{ in}] = 175.4 \text{ k}$

(ii)  $\phi R_n = 0.85 \phi R_{wx} + 1.5 \phi R_{wt} = 4.176 \text{ k/in} [0.85 (2) (16 \text{ in}) + 1.5 (10 \text{ in})] = 176.2 \text{ k}$

CHECK MINIMUM WELD SIZE

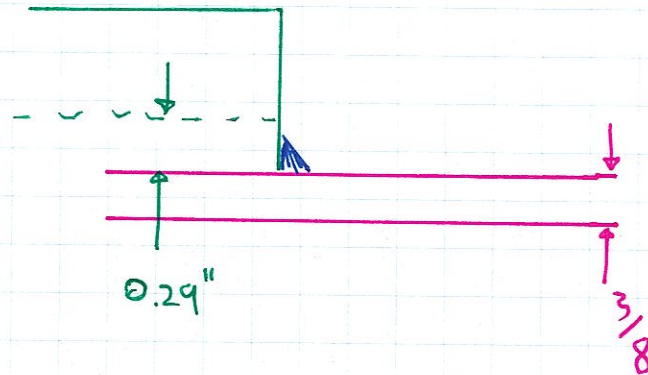
Table J2-4, p16.1-119

$t_{min} = \min (t_{pl} = \frac{3}{8} \text{ in} = 0.375 \text{ in}; t_w = 0.29 \text{ in})$

web of channel



allowed to use larger

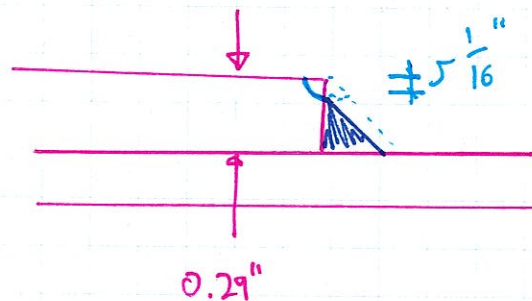


$$t_{\min} = 0.29'' \rightarrow W_{\min} = \frac{3}{16}'' \quad \checkmark$$

### CHECK MAX WELD SIZE

$$\text{trans. weld} \rightarrow t_{\text{web}} = 0.29''$$

$$W_{\max} = 0.29'' - \frac{1}{16}'' = 0.228''$$



$$W = \frac{3}{16}'' = 0.188'' \leq W_{\max} = 0.228'' \quad \checkmark$$