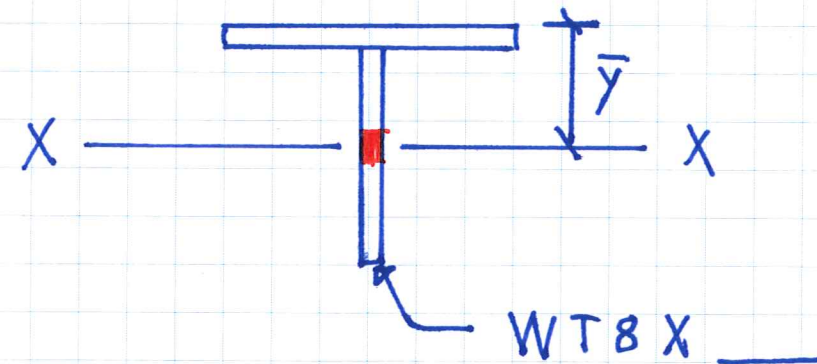
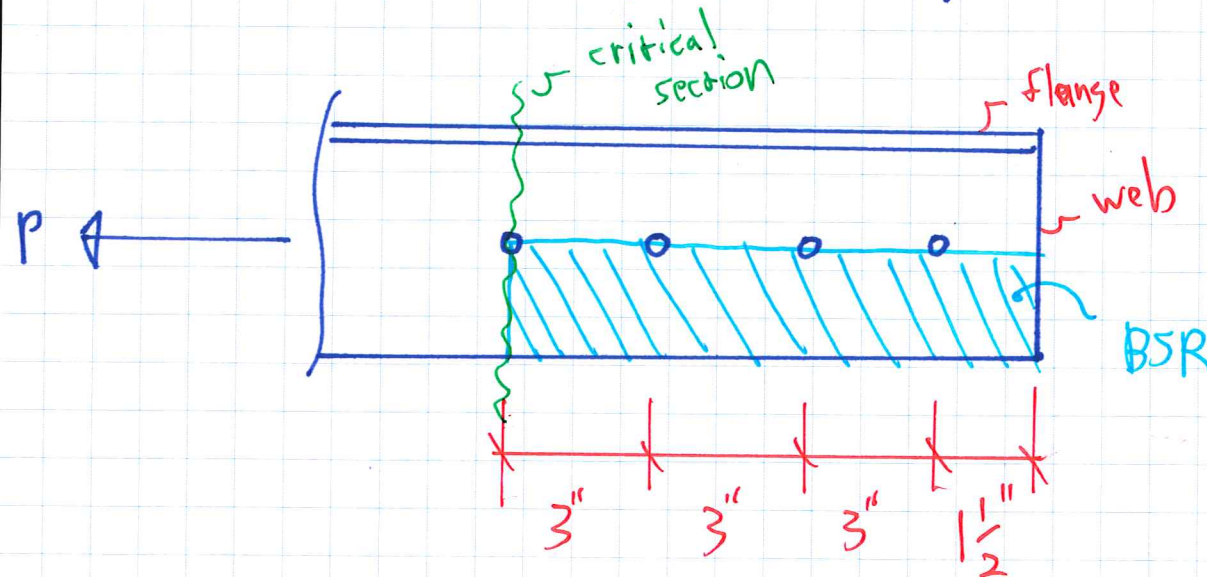


EXAMPLE

GIVEN: A WT Section, A36 Steel, is to carry service tension loads: $PL = 24^k$
 $LL = 80^k$



Member is 12 ft Long

REQD Select the lightest WT8 to carry the load

Use $\frac{3}{4}$ " ϕ bolts

SOLN: By inspection: $P_u = 1.2 D + 1.6 L = 1.2(24) + 1.6(80) = 156.8^k$

$$(A_g)_{\text{reqd}} = \frac{P_u}{\phi f_y} = \frac{156.8^k}{0.9 (36 \text{ ksi})} = 4.84 \text{ in}^2$$

A36: $f_y = 36 \text{ ksi}$
 $f_u = 58 \text{ ksi}$

try WT8X18: $A_g = 5.29 \text{ in}^2$ $\geq (A_g)_{\text{reqd}} = 4.84 \text{ in}^2$ $\therefore$ GSY is ok
 $t_w = 0.295 \text{ in}$
 $\bar{y} = 1.88 \text{ in}$
 $r_{\min} = 1.52 \text{ in}$

NSR: $\phi P_n = \phi A_e f_u$

$$A_n = A_g - \sum A_{\text{holes}} = 5.29 \text{ in}^2 - (1 \text{ hole}) \left(\frac{3}{4}'' + \frac{1}{8}'' \right) (0.295'') = 5.032 \text{ in}^2$$

$$A_e = U A_n = 0.7 (5.032 \text{ in}^2) = 3.522 \text{ in}^2$$

↑
Discrete Value, Table ~~D3.1~~ ^{D3.1}, Case #7

$$\phi P_n = 0.75 (3.522 \text{ in}^2) (58 \text{ ksi}) = 153.2^k \quad \times \quad 156.8^k$$

try
WT 8 x 20:

$$\underline{GSY}: \phi P_n = 191^k > P_u = 156.8^k \quad \checkmark$$

$$\underline{NSR}: \phi P_n = 171^k > P_u = 156.8^k \quad \checkmark$$

$$\underline{BSR}: \phi P_n = 128.4^k < P_u = 156.8^k \quad \underline{X}$$

$$(t_w)_{\text{new}} \approx (t_w)_{\text{old}} \left(\frac{P_u}{P_{BSR}} \right) \approx (0.305") \left(\frac{156.8^k}{128.4^k} \right) \approx 0.372 \text{ in}$$

↑
WT 8 x 20

try
WT 8 x 25:

$$A_g = 7.37 \text{ in}^2$$

$$d = 8.13 \text{ in}$$

$$t_w = 0.380 \text{ in}$$

$$r_{\min} = 1.59 \text{ in}$$

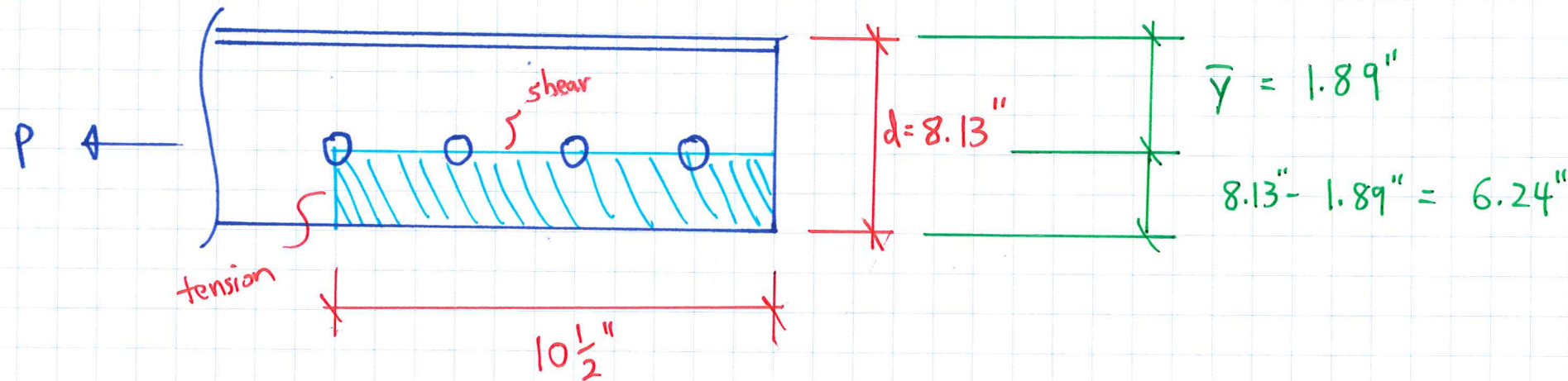
GSY: $\phi P_n = 0.9(36 \text{ ksi})(7.37 \text{ in}^2) = \underline{283.8}^k \geq P_u \quad \checkmark$

NSR: $\phi P_n = \cancel{0.7(0.75)A_n} \quad 0.75 A_e f_u$

$A_e = U A_n = 0.7 \left(7.37 \text{ in}^2 - \left(\frac{3}{4}'' + \frac{1}{8}'' \right) (0.38'') \right) = 4.926 \text{ in}^2$

$\phi P_n = 0.75(4.926 \text{ in}^2)(58 \text{ ksi}) = \underline{214.3}^k \geq P_u \quad \checkmark$

BSR:



$$A_{nt} = (0.38") \left(6.24" - (0.5 \text{ hole}) \left(\frac{3}{4}" + \frac{1}{8}" \right) \right) = 2.205 \text{ in}^2$$

$$A_{gv} = (10.5") (0.38") = 3.99 \text{ in}^2$$

$$A_{nv} = A_{gv} - \sum A_{\text{holes}} = 3.99 - (3.5 \text{ holes}) \left(\frac{3}{4}" + \frac{1}{8}" \right) (0.38") = 2.826 \text{ in}^2$$

$$\phi P_n = \phi [0.6 F_u A_{nt} + U_{bs} F_u A_{nt}] \leq \phi [0.6 F_y A_{gv} + U_{bs} F_u A_{nt}]$$

$$\phi P_n = \underline{160.6}^k \geq P_u = 156.8^k \quad \checkmark$$

Check Slenderness:

$$\frac{L}{r_{\min}} = \frac{(12 \text{ ft})(12) \overset{\text{conversion ft-to-inch}}{\text{}}} {(1.59 \text{ in})} = 90.6 < 300 \quad \checkmark$$